



# High-surface-area ceria prepared by ALD on Al<sub>2</sub>O<sub>3</sub> support



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## ABSTRACT

Al<sub>2</sub>O<sub>3</sub> powders were modified by Atomic Layer Deposition (ALD) of CeO<sub>2</sub> to produce composite catalyst supports for Pd. The weight of the support was found to increase linearly with the number of ALD cycles. This, together with TEM images, indicated that the CeO<sub>2</sub> grows as a dense, conformal film, with a growth rate of 0.02 nm per cycle. The films showed good thermal stability under oxidizing conditions. XRD measurements on a sample with 0.28 g CeO<sub>2</sub>/g Al<sub>2</sub>O<sub>3</sub> showed no evidence for crystalline CeO<sub>2</sub> until calcination above 1073 K. Water-gas-shift rates on 1-wt% Pd catalysts supported on the CeO<sub>2</sub> ALD-modified Al<sub>2</sub>O<sub>3</sub> were essentially identical to rates on conventional Pd-CeO<sub>2</sub> catalysts and much higher than rates on a catalyst in which Pd was supported on Al<sub>2</sub>O<sub>3</sub> with CeO<sub>2</sub> added by infiltration. The WGS rates, together with results from FTIR and CO-O<sub>2</sub> pulse studies, suggest that all of the Pd is in contact with CeO<sub>2</sub> on the ALD-prepared supports and that it should be possible to prepare high-surface-area, functional supports using ALD.

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## 1. Introduction

The ability of ceria to undergo facile oxidation and reduction makes it effective as an Oxygen Storage Capacitor (OSC) in automotive, three-way catalysts [1–7]. The redox properties are also responsible for promotion of rates on ceria-supported metals for the CO-oxidation [8], water-gas-shift [9–12], methane-steam-reforming [13,14], and methane-oxidation [15] reactions. For CO oxidation, the rate enhancements were shown to depend on the interfacial contact between the ceria and the metal [16], implying that direct contact between the two phases is essential. Unfortunately, the stability of ceria is a problem. In automotive applications, ceria readily crystallizes and sinters, “with growth of particles and loss of surface area, leading to rapid reduction of the oxygen storage and release properties” [17]. Hydrothermal aging and the resulting increase in ceria crystallinity have also been shown to change the thermodynamics of CeO<sub>2</sub> reduction, increasing the magnitude of the heat of oxidation by as much as 50% [18].

Various strategies are used to stabilize the ceria component. First, the OSC component in three-way catalysts is always in the

form of a CeO<sub>2</sub>-ZrO<sub>2</sub> mixed oxide [19]. These mixed oxides still lose most of their surface area after thermal treatments [20] but the mixed oxides remain thermodynamically reducible. The heats of oxidation for CeO<sub>2</sub>-ZrO<sub>2</sub> mixed oxides do not significantly change with particle size or surface area [21,22]. However, a high surface area for the ceria component is still important for maintaining contact with the transition metal. One strategy to stabilize the surface area of the OSC component involves incorporating alumina particles as diffusion barriers to prevent contact between adjacent CeO<sub>2</sub>-ZrO<sub>2</sub> particles [17]. This approach has been shown to be effective in maintaining surface areas but introduces difficulties in that the supported metals may not be in contact with the ceria-containing component.

In the present work, we set out to synthesize a composite support of ceria on high-surface-area Al<sub>2</sub>O<sub>3</sub> using Atomic Layer Deposition (ALD). While conventional infiltration of Al<sub>2</sub>O<sub>3</sub> with Ce(NO<sub>3</sub>)<sub>3</sub> solutions, followed by heating to decompose the nitrate ions, forms CeO<sub>2</sub> crystallites that cover only a fraction of the surface, ALD is in principle capable of forming uniform, atomic-scale films that cover the entire Al<sub>2</sub>O<sub>3</sub> surface. This morphology maximizes the interfacial contact between ceria and any metal catalyst that is introduced to the support. The Al<sub>2</sub>O<sub>3</sub> could also stabilize the ceria surface area and prevent crystallite growth, depending on the relative interfacial energies between CeO<sub>2</sub> and Al<sub>2</sub>O<sub>3</sub>.

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ALD is a self-limiting process in which films are produced through repeated cycles of reaction between an organometallic precursor and the substrate of interest, followed by oxidation. Reaction of the precursor with the surface is carried out under conditions which limit the reaction to one monolayer, so that the thickness of the final oxide film can be precisely controlled and determined by the number of cycles. Although ALD has found application primarily for fabrication of semiconductor devices, it has also been used in the synthesis of heterogeneous catalysts. For example, ALD has been used to prepare well-dispersed metal particles [23–25] and to stabilize supported-metal particles by “over” coating with an inert oxide film [26–28]. Review papers on the application of ALD to heterogeneous catalysis are available [29–31]. The main issue with using ALD in catalyst preparation is that there can be diffusional limitations with the organometallic precursor when the films are deposited on high-surface-area supports; however, previous work has shown that this can be prevented by using long exposure times in a static system [32,33].

In this paper, we will demonstrate that it is possible to prepare a  $\text{CeO}_2/\text{Al}_2\text{O}_3$  composite support in which  $\text{CeO}_2$  exists as a thin film on top of the  $\text{Al}_2\text{O}_3$ . We will also show that this composite support has similar catalytic properties to what would be expected for a high-surface-area  $\text{CeO}_2$  support, but with better stability.

## 2. Experimental methods

Atomic Layer Deposition (ALD) of  $\text{CeO}_2$  was performed using a deposition system that has been described in detail in previous publications [32,33]. The system consists of several heated chambers for the substrate, the organometallic precursor, and tubing between the substrate and the precursor, all of which could be evacuated to  $\sim 10^{-3}$  Torr using a mechanical vacuum pump. High-temperature valves separated the substrate chamber from the precursor chamber and from both the vacuum pump and the oxygen source. After evacuation, the precursor, Tetrakis (2,2,6,6-tetramethyl-3,5-heptanedionato) cerium,  $(\text{Ce}(\text{TMHD})_4)$ , Strem Chemicals, Inc.), was heated to 453 K to produce a vapor pressure of approximately 2 Torr. During the deposition cycle, the  $\text{Ce}(\text{TMHD})_4$  vapor was introduced to the evacuated sample chamber containing approximately 0.5-g  $\text{Al}_2\text{O}_3$ . The alumina substrate was exposed to the precursor vapor at 503 K for 300 s to ensure that the reaction with the surface was complete. Because a previous study showed that the  $\text{Ce}(\text{TMHD})_4$  precursor may not be completely oxidized at 503 K [34], in the present study, we removed the sample from the ALD system after evacuation and then heated it to 673 K in a muffle furnace for 5 min between exposures to the  $\text{Ce}(\text{TMHD})_4$  precursor.

The substrate in this study was a  $\gamma\text{-Al}_2\text{O}_3$  (Strem Chemicals, Inc.) that had been stabilized by calcining in air to 1173 K for 24 h. The BET surface area after this pretreatment was  $130\text{ m}^2/\text{g}$ . To characterize film growth during ALD, gravimetric analysis was performed after every 5 ALD cycles. To benchmark the properties of this composite support, catalysts were also prepared using the unmodified  $\text{Al}_2\text{O}_3$ , the same  $\text{Al}_2\text{O}_3$  with  $0.28\text{ g CeO}_2/\text{g Al}_2\text{O}_3$  added by infiltration with aqueous solutions of cerium (III) nitrate hexahydrate ( $10\text{ g, Ce}(\text{NO}_3)_3 \cdot 6\text{H}_2\text{O}$ , Sigma Aldrich) (Referred to here as  $\text{CeO}_2(\text{IMP})/\text{Al}_2\text{O}_3$ ), and a bulk  $\text{CeO}_2$  powder. The  $\text{CeO}_2(\text{IMP})/\text{Al}_2\text{O}_3$  was calcined to 673 K for 6 h to remove any nitrates. The  $\text{CeO}_2$  powder was prepared by precipitating an aqueous solution of  $\text{Ce}(\text{NO}_3)_3 \cdot 6\text{H}_2\text{O}$  with excess ammonium hydroxide ( $\text{NH}_4\text{OH}$ , Fisher Scientific), as described in a previous publication [32].

All of the 1-wt% Pd catalysts were prepared by incipient wetness using an aqueous solution of tetraaminopalladium(II) nitrate (Sigma Aldrich). The materials were then dried overnight at 333 K and calcined at 773 K in air for 6 h to remove any organics and nitrates. The elemental compositions of the samples were

measured by Inductively Coupled Plasma-Optical Emission spectrometry (ICP-OES) performed on a Spectro Genesis spectrometer with a concentric nebulizer. For the ICP-OES measurement, each sample ( $\sim 50\text{ mg}$ ) was dissolved in a 5 mL solution of Aqua Regia overnight. The solutions were then diluted with a 10 wt.%  $\text{HNO}_3$  solution to the appropriate concentration before the ICP analysis. The Pd dispersions were determined volumetrically using CO adsorption uptakes at room temperature on the reduced catalysts [10]. In this procedure, the samples were first oxidized in 200 Torr  $\text{O}_2$  at 673 K and reduced in 200 Torr  $\text{H}_2$  at 423 K before measuring CO uptakes. Dispersions were calculated assuming one CO per surface Pd. Sample surface areas were determined from BET isotherms using  $\text{N}_2$  adsorption at 78 K. X-Ray Diffraction (XRD) patterns were recorded on a Rigaku Smartlab diffractometer equipped with a  $\text{Cu K}\alpha$  source ( $\lambda = 0.15416\text{ nm}$ ).

*Ex-situ* scanning transmission electron microscopy (STEM) was performed on powder specimens that had been sonicated in methanol and dropped onto carbon support films on copper TEM grids (Ted Pella, Inc.) for TEM examination. Specimens were examined with a JEOL 3100R05 electron microscope with double spherical aberration-correctors operated at 300 kV in scanning mode.

Steady-state water-gas-shift reaction rates were measured in a 0.25-inch, quartz, tubular reactor as the carrier gas with partial pressures of CO and  $\text{H}_2\text{O}$  both at 25 Torr (3.3%). The total flow rate of He was kept at 60 mL/min. Before testing, each sample was activated by heating the catalysts to 673 K in the reaction mixture before cooling back to the desired reaction temperature. The light-off profile CO-oxidation rates were also determined in the same flow reactor with CO and  $\text{O}_2$  being 25 and 12.5 Torr, respectively, and the balance being He. The total flow rate of the gas mixture was maintained at  $120\text{ mL min}^{-1}$ . The samples tested for CO oxidation were previously heated to 1073 K in air before testing. The mass of catalyst used in every rate measurement was 0.10 g and the products were analyzed using a gas chromatograph (SRI8610C) equipped with a Haysep Q column and a TCD detector. All rates in this study were normalized to the mass of the catalyst. Differential conversions were maintained in all cases.

Fourier Transform Infrared (FTIR) spectra were collected on a Mattson Galaxy FTIR with a diffuse-reflectance attachment (Collector II<sup>TM</sup>) purchased from Spectra-Tech Inc. Spectra were collected at  $4\text{ cm}^{-1}$  resolution. The intensities of the spectral features were normalized by making the background peaks between  $700\text{ cm}^{-1}$  and  $1000\text{ cm}^{-1}$  be identical for all cases.

The transient-pulse experiments were performed using a system that has been described in other publications [35,36]. The system consists of a tubular reactor equipped with computer-controlled solenoid valves to allow step changes in the composition of the inlet gases. Reactant gases were passed over 200-mg samples in a 1/4-inch quartz tube. The reactor effluent was monitored continuously using an online quadrupole mass spectrometer. The total flow rate with He as the carrier gas was kept constant at 25 mL/min, while the concentrations of the reactive component (either CO or  $\text{O}_2$ ) was chosen to be 10% of the total gas stream. Integration of the partial pressures as a function of time allowed accurate determination of the amounts of  $\text{CO}_2$  formed during a CO pulse. Prior to taking the pulse data, we first calcined the samples in 10%  $\text{O}_2$  at 673 K for 15 min. This was followed by reduction in 10% CO in Helium at 673 K for 10 min and then re-oxidation in 10%  $\text{O}_2$  for an additional 15 min. No attempt was made to analyze the shapes of the pulses because coupling between desorption, re-adsorption, reaction, and diffusion does not allow for a unique determination of rate processes in transient experiments of this type.

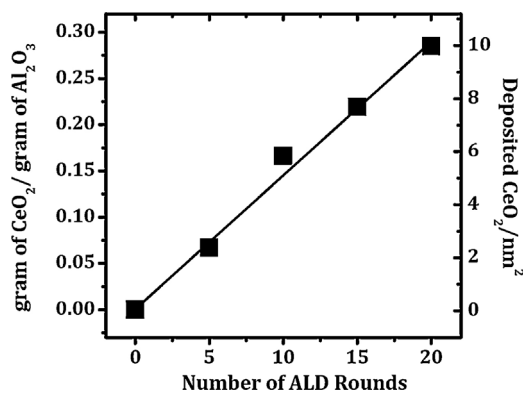


Fig. 1. Mass change as a function of the number of  $\text{CeO}_2$  ALD cycles on an  $\text{Al}_2\text{O}_3$  support which had an initial surface area of  $130 \text{ m}^2/\text{g}$ .

### 3. Results

#### 3.1. Characterization of $\text{CeO}_2$ films on $\text{Al}_2\text{O}_3$

The growth rates for the  $\text{CeO}_2$  films on  $\text{Al}_2\text{O}_3$  were determined gravimetrically by measuring the sample mass after every 5 ALD cycles, with results shown in Fig. 1. Similar to what we reported earlier for growth of  $\text{ZrO}_2$  films by ALD on a similar alumina substrate, we observed that the sample weight increased linearly with the number of cycles. After 20 cycles, the sample (Referred to here as  $20\text{CeO}_2\text{-Al}_2\text{O}_3$ ) had a total weight gain of approximately  $0.28 \text{ g CeO}_2/\text{g Al}_2\text{O}_3$ . That this weight increase corresponded to  $\text{CeO}_2$  was confirmed by ICP analysis. Assuming that ceria forms a uniform, dense film with the bulk properties of  $\text{CeO}_2$  over the  $130\text{-m}^2/\text{g Al}_2\text{O}_3$  surface, a  $0.28 \text{ g CeO}_2/\text{g Al}_2\text{O}_3$  loading of  $\text{CeO}_2$  corresponds to a film thickness of  $0.4 \text{ nm}$  ( $(0.28 \text{ g CeO}_2/\text{g Al}_2\text{O}_3) \times (1 \text{ cm}^3/7.21 \text{ g CeO}_2) \times (1 \text{ g Al}_2\text{O}_3/130 \text{ m}^2) \times (1 \text{ m}^2/10^4 \text{ cm}^2) \times (10^7 \text{ nm/cm})$ ). The growth rate calculated from this loading,  $0.02 \text{ nm/cycle}$ , is identical to the value that has been reported in the literature for this precursor on flat substrates [37] and similar to what was observed previously for  $\text{ZrO}_2$  film growth on a similar alumina substrate [32,33].

In order to verify the presence of a thin  $\text{CeO}_2$  film, high angle annular dark field (HAADF) STEM imaging was used to characterize the  $20\text{CeO}_2\text{-Al}_2\text{O}_3$  sample, as shown in Fig. 2(a) through (d). Due to the atomic number difference between Ce and Al,  $\text{CeO}_2$  appears brighter so the surface layer is distinguishable. The images in Fig. 2(a) and (b) were obtained on the fresh sample calcined at  $673 \text{ K}$  and show that the  $\text{Al}_2\text{O}_3$  is covered by a relatively uniform  $\text{CeO}_2$  film with a thickness close to the expected  $0.4\text{-nm}$ . Not surprisingly for deposition on curved surfaces, some slightly larger  $\text{CeO}_2$  particles are observed at the higher magnification. The images in Figs. 2(c) and (d) show the same sample after calcination to  $1073 \text{ K}$ . Under low magnification, Fig. 2(c), the entire surface of the support still appears to be covered with  $\text{CeO}_2$ . However, small particles, less than  $5\text{-nm}$  in size, were also observed at high magnification, Fig. 2(d), along with areas that still show the presence of a  $\text{CeO}_2$  film.

The morphology of the  $20\text{CeO}_2\text{-Al}_2\text{O}_3$  sample was clearly different from that of the  $\text{CeO}_2(\text{IMP})/\text{Al}_2\text{O}_3$  sample, obtained by infiltration with aqueous solutions  $\text{Ce}(\text{NO}_3)_3$  onto the same  $\text{Al}_2\text{O}_3$ . The images in Figs. 2(e) and (f) were obtained on  $\text{CeO}_2(\text{IMP})/\text{Al}_2\text{O}_3$ , which had the same weight loading of  $\text{CeO}_2$ , after calcination to  $673 \text{ K}$ . The images show that the  $\text{CeO}_2$  exists as  $20\text{-nm}$  clusters of roughly  $3\text{-nm}$  particles, even after this low calcination temperature. Furthermore, most of the  $\text{Al}_2\text{O}_3$  remains uncovered by  $\text{CeO}_2$ . It should be acknowledged that we did not attempt to optimize the impregnation procedure to maximize the  $\text{CeO}_2$  dispersion.

Table 1

BET Surface Area as a function of Calcination Temperature. The surface area of the Alumina support is  $130 \text{ m}^2/\text{g}$ .

Calcination Temperature (K)	BET Surface Area ( $\text{m}^2/\text{g}$ )		
	Pd/CeO <sub>2</sub>	Pd/20CeO <sub>2</sub> -Al <sub>2</sub> O <sub>3</sub>	Pd/CeO <sub>2</sub> (IMP)/Al <sub>2</sub> O <sub>3</sub>
773	42	82	110
973	30	78	100
1073	18	84	100

Table 2

Dispersion Measurement as a function of Calcination Temperature.

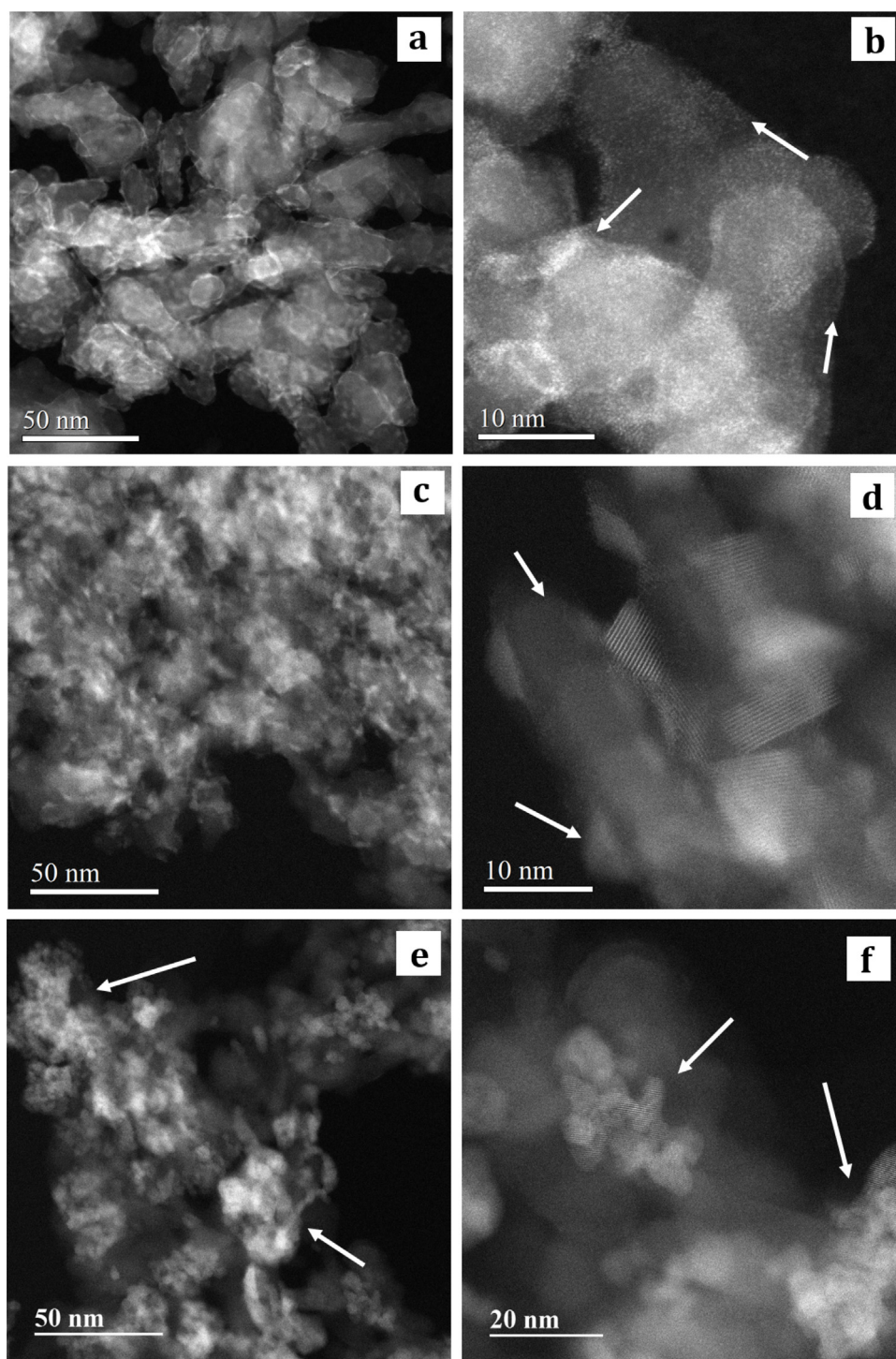
Calcination Temperature (K)	Dispersion (%)		
	Pd/CeO <sub>2</sub>	Pd/20CeO <sub>2</sub> -Al <sub>2</sub> O <sub>3</sub>	Pd/Al <sub>2</sub> O <sub>3</sub>
773	40	65	34
973	35	63	30
1073	30	59	24

XRD patterns of the  $20\text{CeO}_2\text{-Al}_2\text{O}_3$  sample are shown as a function of calcination temperature in Fig. 3, together with the pattern for the untreated  $\text{Al}_2\text{O}_3$ , Fig. 3(a) and the pattern for the  $\text{CeO}_2(\text{IMP})/\text{Al}_2\text{O}_3$  sample, Fig. 3(e). First, it is worth noting that the diffraction pattern of the infiltrated sample with the same  $\text{CeO}_2$  loading and calcined to only  $673 \text{ K}$ , Fig. 3(e), is very different. The peaks associated with  $\text{CeO}_2$  dominate on  $\text{CeO}_2(\text{IMP})/\text{Al}_2\text{O}_3$ , to the point that the peaks from  $\text{Al}_2\text{O}_3$  are difficult to see on the same scale due to the larger X-Ray scattering cross section for Ce compared to Al. Even for this relatively low calcination temperature, the  $\text{CeO}_2$  domain size, calculated using the Scherrer Equation and the peak width at  $28^\circ 2\theta$ , was already  $10 \text{ nm}$ . By comparison, there is no evidence for the presence of  $\text{CeO}_2$  in the  $20\text{CeO}_2\text{-Al}_2\text{O}_3$  from the diffraction results after calcination at  $873 \text{ K}$ , Fig. 3(b). This is consistent with the fact that the domain size for ceria in these samples is very small. Features associated with  $\text{CeO}_2$  begin to appear near  $28$  and  $58^\circ 2\theta$  in the diffraction pattern of the sample calcined to  $1073 \text{ K}$ , Fig. 3(c), and become more prominent after calcination at  $1173 \text{ K}$ , Fig. 3(d). However, the intensity of the  $\text{CeO}_2$  peaks remains weak, implying that much of the  $\text{CeO}_2$  is not contributing. Based on diffraction peak widths, the crystallite size of  $\text{CeO}_2$  particles was only  $8 \text{ nm}$ , even after calcination to  $1173 \text{ K}$ .

#### 3.2. Catalytic properties

To determine how modification of the  $\text{Al}_2\text{O}_3$  support by  $\text{CeO}_2$  ALD affects the catalyst-support properties, we examined a series of  $1\text{-wt}\%$  Pd catalysts prepared from the unmodified  $\text{Al}_2\text{O}_3$ , from the  $\text{CeO}_2$  powder, from the  $\text{CeO}_2(\text{IMP})/\text{Al}_2\text{O}_3$  sample, and from the  $20\text{CeO}_2\text{-Al}_2\text{O}_3$  sample. It is first interesting to compare the BET surface areas of  $1\text{-wt}\%$  Pd/ $\text{CeO}_2$  powder and  $1\text{-wt}\%$  Pd/ $20\text{CeO}_2\text{-Al}_2\text{O}_3$  as a function of calcination temperature. These results are reported in Table 1. Because the  $\gamma\text{-Al}_2\text{O}_3$  used here was initially heated to  $1173 \text{ K}$ , its surface area was only  $130 \text{ m}^2/\text{g}$ . The addition of  $20$  cycles of  $\text{CeO}_2$  by ALD and of  $1\text{-wt}\%$  Pd by infiltration reduced this to  $82 \text{ m}^2/\text{g}$ . Most of this decrease in specific surface area can be accounted for by the addition of  $0.28\text{-g CeO}_2$  and  $0.01\text{-g Pd}$  per gram of catalyst ( $130 \text{ m}^2/1.29 \text{ g} = 100 \text{ m}^2/\text{g}$ ). The additional decrease in specific surface area is likely due to a decreased average pore diameter as the pores of the  $\text{Al}_2\text{O}_3$  are coated with a nonporous,  $0.4\text{-nm}$  film. Calcination of this sample to  $1073 \text{ K}$  had essentially no effect on the surface area. By contrast, the specific surface area of the Pd/ $\text{CeO}_2$  powder decreased from a value of  $46 \text{ m}^2/\text{g}$  after calcination to  $673 \text{ K}$ , to  $42 \text{ m}^2/\text{g}$   $773 \text{ K}$  and  $18 \text{ m}^2/\text{g}$  at  $1073 \text{ K}$ . Pd dispersion measurements were also performed as a function of calcination temperature on the Pd/ $\text{Al}_2\text{O}_3$ , Pd/ $\text{CeO}_2$ , and Pd/ $20\text{CeO}_2\text{-Al}_2\text{O}_3$  samples, with results shown Table 2. The data indicate that there was

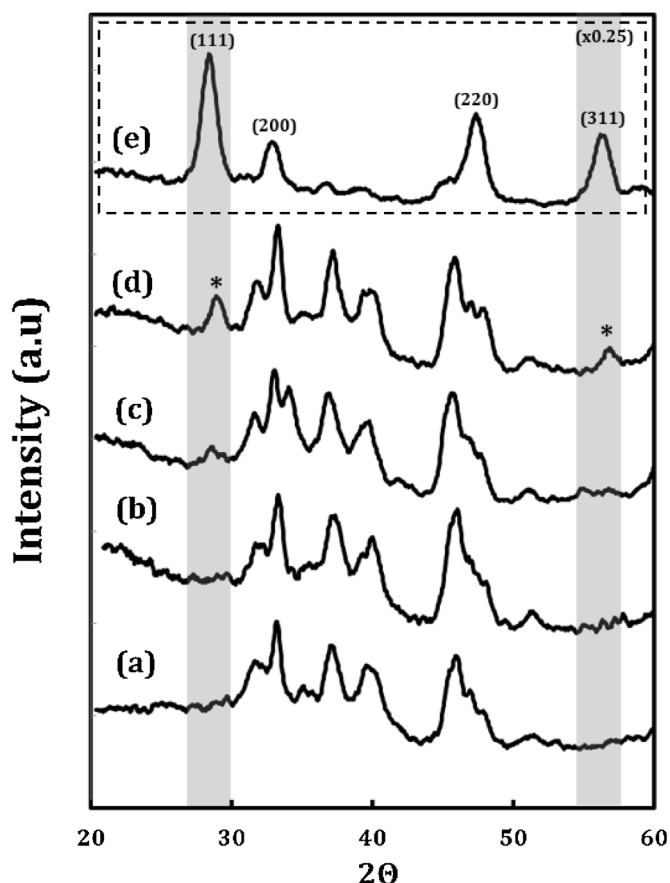




**Fig. 2.** High angle annular dark field STEM image of ALD 20CeO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub> sample after calcination at 673 K (a–b) and 1073 K (c–d), showing that the uniform atomic CeO<sub>2</sub> layer made through ALD deposition evolved into a mixture of 5-nm CeO<sub>2</sub> particles and CeO<sub>2</sub> film after 1073 K calcination. Impregnated samples after calcination at 673 K (e–f) are shown for comparison. CeO<sub>2</sub> particles appear in agglomerates, ~20-nm in size, and do not cover the surface uniformly. Arrows indicate the location of CeO<sub>2</sub>, which appears as the brighter features in all six images.

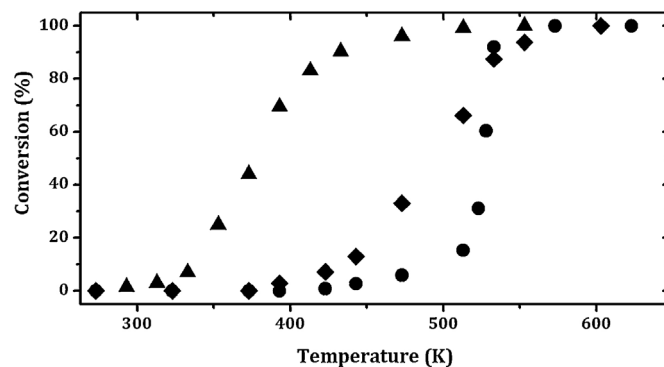
a fairly significant loss of Pd dispersion with calcination temperature on the Pd/Al<sub>2</sub>O<sub>3</sub> sample, from 34% after 773 K and 24% after 1073 K. Given the significant loss in total surface area of Pd/CeO<sub>2</sub>, the decrease in dispersion from 40% to 30% in this temperature range is small, indicating that CeO<sub>2</sub> likely helps maintain dispersion [38]. The Pd dispersion on Pd/20CeO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub> was 65% following catalyst treatment at 773 K and did not change significantly with calcination.

It has been suggested that sites of contact between Pd and ceria are especially active for the WGS reaction due to the ability of reduced ceria to be oxidized by water, then transfer either oxygen or OH to CO that is adsorbed on the Pd [9,10]. Based on this picture, WGS rates provide information about whether Pd is in contact with CeO<sub>2</sub> in composite materials. Therefore, differential WGS rates were measured for the Pd/20CeO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub>, Pd/CeO<sub>2</sub>, Pd/Al<sub>2</sub>O<sub>3</sub> and Pd/CeO<sub>2</sub>(IMP)/Al<sub>2</sub>O<sub>3</sub> catalysts. The data obtained following calci-



**Fig. 3.** XRD patterns of the (a) uncoated  $\text{Al}_2\text{O}_3$  support heated to 1173 K and the ALD-coated,  $20\text{CeO}_2\text{-Al}_2\text{O}_3$  sample after calcination to the following temperatures: (b) 873 K; (c) 1073 K; and (d) 1173 K. The pattern in (e) was obtained on  $\text{CeO}_2(\text{IMP})/\text{Al}_2\text{O}_3$  heated to 673 K. Characteristic peaks for  $\text{CeO}_2$  are marked by the grey line and \*. Peaks were normalized to a distinct  $\text{Al}_2\text{O}_3$  peak at  $2\theta = 46^\circ$ , and the image (e) was scaled by  $\times 0.25$ .

nation of the catalysts to 773 K are shown in Fig. 4(a). Rates on  $\text{Pd}/\text{CeO}_2$  were almost 10 times higher than those on  $\text{Pd}/\text{Al}_2\text{O}_3$ , as expected. What is more interesting is that the differential rates on  $\text{Pd}/\text{CeO}_2$  were nearly indistinguishable from rates on  $\text{Pd}/20\text{CeO}_2\text{-Al}_2\text{O}_3$ . Because the ALD-prepared sample is completely covered with  $\text{CeO}_2$ , its catalytic properties are nearly identical to those of a

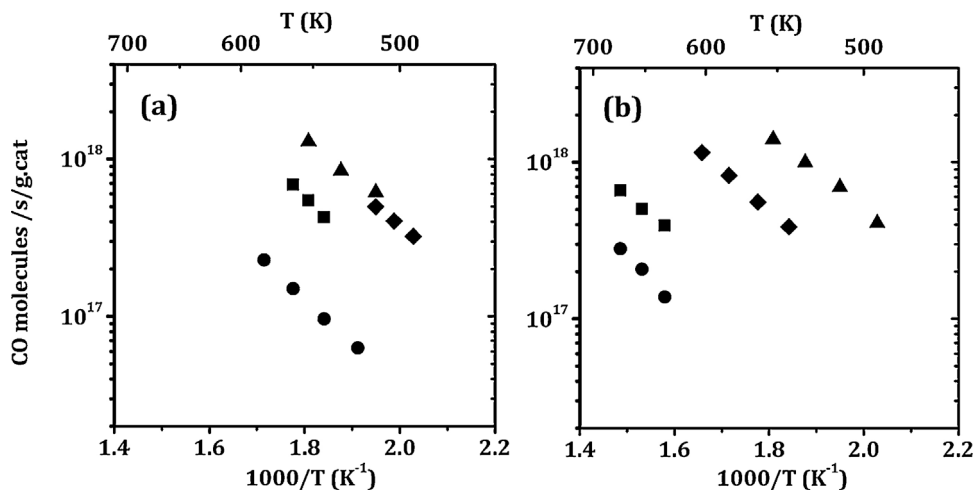


**Fig. 5.** Light-off curves of CO conversion versus temperature for: ( $\blacktriangle$ )  $\text{Pd}/20\text{CeO}_2\text{-Al}_2\text{O}_3$ , ( $\blacklozenge$ )  $\text{Pd}/\text{CeO}_2$ , and ( $\bullet$ )  $\text{Pd}/\text{Al}_2\text{O}_3$  calcined at 1073 K. The CO oxidation reaction was carried out with partial pressures of CO and  $\text{O}_2$  at 25 Torr and 12.5 Torr, respectively.

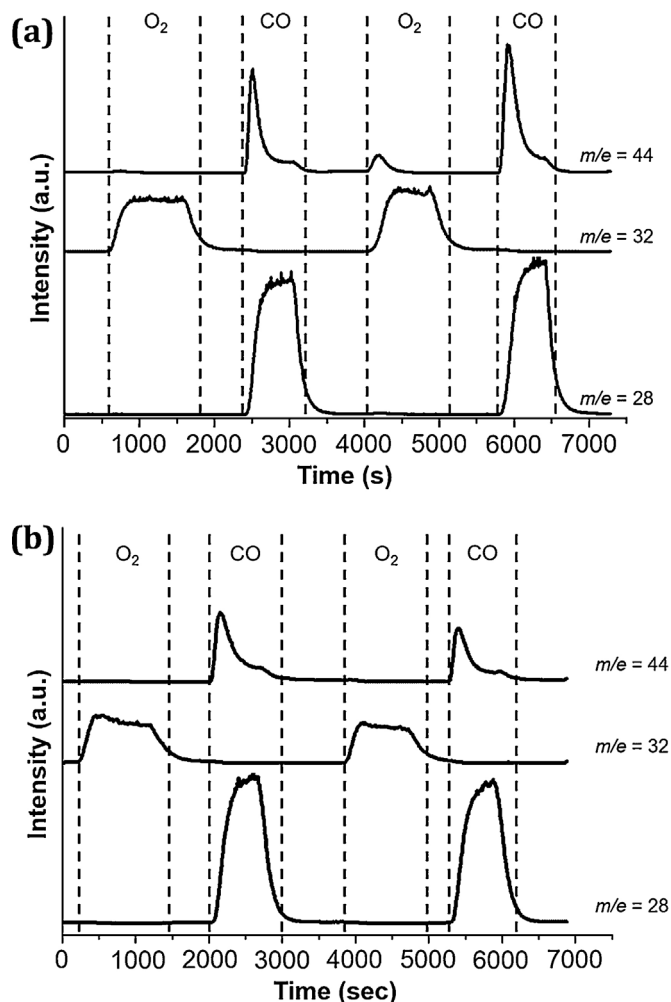
conventional  $\text{CeO}_2$ -supported catalyst. Since the Pd dispersions on  $\text{Pd}/\text{CeO}_2$  and  $\text{Pd}/20\text{CeO}_2\text{-Al}_2\text{O}_3$  are also reasonably close for 773-K calcination, the number of contact sites between Pd and ceria are also similar. Rates on  $\text{Pd}/\text{CeO}_2(\text{IMP})/\text{Al}_2\text{O}_3$  are approximately 2 times lower, probably because some of the Pd particles are not in contact with  $\text{CeO}_2$ .

Larger differences in the WGS rates were observed between the samples after the samples were calcined at 1073 K, as shown in Fig. 4(b). Most significantly, rates on the  $\text{Pd}/20\text{CeO}_2\text{-Al}_2\text{O}_3$  sample remain unchanged. This is consistent with the observations that increased calcination temperature did not affect either the surface area or the Pd dispersion. The fact that the rates remain unchanged implies that contact between Pd and ceria also remains good. Rates on  $\text{Pd}/\text{CeO}_2$  decreased by a factor of about three after heating to higher temperatures, an amount that is too large to be explained entirely by the lower Pd dispersion. Because loss in ceria surface area is associated with an increase in crystallite size and larger ceria crystallites are considered to be less reducible, it is possible that the decrease in rates is associated with a change in the ceria reducibility. An even larger drop in rates occurs with the  $\text{Pd}/\text{CeO}_2(\text{IMP})/\text{Al}_2\text{O}_3$  sample, possibly due to a loss in interfacial contact between the Pd and the ceria component of the support.

To further probe the catalytic properties of these catalysts, we measured light-off rates for CO oxidation on the  $\text{Pd}/20\text{CeO}_2\text{-Al}_2\text{O}_3$ ,  $\text{Pd}/\text{CeO}_2$  and  $\text{Pd}/\text{Al}_2\text{O}_3$  samples after they had been calcined to 1073 K in air. These results are shown in Fig. 5. The light-off tem-



**Fig. 4.** Steady-state, differential reaction rates for water gas shift (WGS) reaction with partial pressure of CO and  $\text{H}_2\text{O}$  both at 25 Torr. WGS rates after pretreatment calcination to (a) 773 K and (b) 1073 K were compared for the following catalysts: ( $\blacktriangle$ )  $\text{Pd}/20\text{CeO}_2\text{-Al}_2\text{O}_3$  ( $\blacklozenge$ )  $\text{Pd}/\text{CeO}_2$ , ( $\blacksquare$ )  $\text{Pd}/\text{CeO}_2(\text{IMP})/\text{Al}_2\text{O}_3$ , and ( $\bullet$ )  $\text{Pd}/\text{Al}_2\text{O}_3$ .



**Fig. 6.** Pulse measurements on (a) Pd/20CeO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub>, and (b) Pd/Al<sub>2</sub>O<sub>3</sub> catalysts at 673 K. The data are for two rounds of CO pulse ( $m/e = 28$ ) and of O<sub>2</sub> pulse ( $m/e = 32$ ). Formation of CO<sub>2</sub> ( $m/e = 44$ ) is observed.

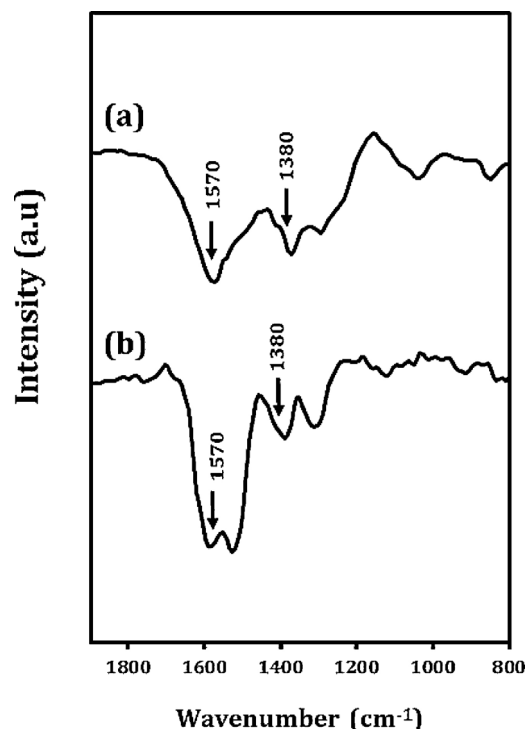
**Table 3**

Redox data for the pulse-reactor measurements performed at 673 K using CO-O<sub>2</sub> pulses over the samples.

Sample	Average CO <sub>2</sub> ( $\mu\text{mol/g}$ ) formed from CO pulse
Pd/20CeO <sub>2</sub> -Al <sub>2</sub> O <sub>3</sub>	220
Pd/CeO <sub>2</sub>	160
Pd/Al <sub>2</sub> O <sub>3</sub>	87

peratures correspond reasonably well with the relative WGS rates. The Pd/20CeO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub> sample was by far the most active, followed by the Pd/CeO<sub>2</sub> and Pd/Al<sub>2</sub>O<sub>3</sub> samples. Again, the higher rates on Pd/20CeO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub> are an indication of good contact between Pd and ceria.

The redox properties of Pd/20CeO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub>, Pd/CeO<sub>2</sub> and Pd/Al<sub>2</sub>O<sub>3</sub> samples were probed using alternating CO and O<sub>2</sub> pulses at 673 K. Fig. 6 shows a comparison of results for the Pd/20CeO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub> and Pd/Al<sub>2</sub>O<sub>3</sub> catalysts, while a summary of the quantities of oxygen that could be added and removed from the samples is reported in Table 3. In Fig. 6, the regions between the dashed lines correspond to when either 10% O<sub>2</sub> ( $m/e = 32$ ) or 10% CO ( $m/e = 28$ ) was added to the He passing over the catalyst. The observation of CO<sub>2</sub> ( $m/e = 44$ ) upon exposure of the catalyst to CO is due to reduction of the catalyst. Formation of CO<sub>2</sub> during the O<sub>2</sub> pulse on Pd/20CeO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub>, but not on Pd/Al<sub>2</sub>O<sub>3</sub>, sample is due to decomposition of carbonates that form on reduced ceria [10]. In the



**Fig. 7.** DRIFTS spectra obtained for (a) Pd/CeO<sub>2</sub> and (b) Pd/20CeO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub>, after exposure to 10% CO in flowing He at 573 K for 10 min.

calculation of oxygen capacitance, the CO<sub>2</sub> from both the CO and O<sub>2</sub> pulses were added in determining the capacitance. A sample with 1-wt% Pd can provide 94  $\mu\text{mol/g}$  of atomic oxygen by reduction of PdO. For bulk CeO<sub>2</sub>, complete reduction to Ce<sub>2</sub>O<sub>3</sub> removes 2900  $\mu\text{mol/g}$  of oxygen. The amounts oxygen removed from the Pd/Al<sub>2</sub>O<sub>3</sub> sample, 87  $\mu\text{mol/g}$  of CO<sub>2</sub>, are within experimental error of the amount expected. Results for Pd/20CeO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub> and Pd/CeO<sub>2</sub> were similar, forming 220 and 160  $\mu\text{mol/g}$  of CO<sub>2</sub> respectively. In both cases, the ceria in contact with the Pd must be undergoing oxidation and reduction.

Finally, in order to compare the surface chemistry of 20CeO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub> and bulk CeO<sub>2</sub>, we performed FTIR measurements on the Pd/ceria and Pd/20CeO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub> catalysts after they had been reduced in 10% CO-He mixtures. As mentioned above, this treatment is expected to reduce the ceria surface and form carbonates. As shown by the spectra in Fig. 7, this is exactly what is observed on both samples. Both samples exhibit broad features between 1300 and 1700  $\text{cm}^{-1}$  that correspond to the carbonates. Because absorption in the IR region is strong on bulk CeO<sub>2</sub>, the spectrum on Pd/20CeO<sub>2</sub>-Al<sub>2</sub>O<sub>3</sub> is simpler. The results suggest that the ALD-modified sample could be a convenient, model system for spectroscopic characterization.

#### 4. Discussion

The present results indicate that it is possible to prepare a support material with the catalytic, promotional properties of ceria by depositing a thin conformal layer of CeO<sub>2</sub> onto a high-surface-area Al<sub>2</sub>O<sub>3</sub> using Atomic Layer Deposition. When used as a support for Pd, the thin CeO<sub>2</sub> film has a similar effect on the water-gas-shift and CO-oxidation reactions as bulk CeO<sub>2</sub>. The ALD-modified support has advantages over bulk ceria in that the underlying Al<sub>2</sub>O<sub>3</sub> provides surface area for the CeO<sub>2</sub> and stabilizes that area to high-temperature calcination.

The thin-film, CeO<sub>2</sub>-coated Al<sub>2</sub>O<sub>3</sub> morphology would be difficult to achieve using conventional methods. With normal infiltration



of Ce salts onto  $\text{Al}_2\text{O}_3$ , particles tend to form clusters during the drying or precipitation steps. Similarly, co-precipitation of alumina and ceria will tend to form a mixture of particles in which a large fraction of the surface will be  $\text{Al}_2\text{O}_3$ . As we have seen in the present study, these materials are not as effective as bulk  $\text{CeO}_2$ , probably because supported metals will distribute between the  $\text{Al}_2\text{O}_3$  and  $\text{CeO}_2$  phases. In this regard, ALD may be unique in providing this hierarchical structure.

The  $\text{CeO}_2$  films that were formed by ALD showed surprising good thermal stability upon calcination. Even after calcination to 1173 K, the diffraction peaks for  $\text{CeO}_2$  were weak compared to what was observed for a  $\text{CeO}_2/\text{Al}_2\text{O}_3$  formed by infiltration with a similar  $\text{CeO}_2$  loading. It is possible that spatial isolation is responsible for maintaining the small crystallites but surface energies may also be responsible. Although  $\text{CeO}_2$  does not react with  $\text{Al}_2\text{O}_3$ ,  $\text{Ce}^{+3}$  can form a  $\text{CeAlO}_3$  perovskite structure. It is therefore possible that there could be bonding interactions at the  $\text{CeO}_2$ - $\text{Al}_2\text{O}_3$  interface. High-temperature reducing conditions could be a problem if compound formation were to occur.

Finally, it is interesting to note that the ALD approach for making “coated” supports is quite general and could be used to make other high-surface-area, functional supports. This opens up a number of opportunities. An obvious extension to the work in this paper would be to prepare  $\text{CeO}_2$ - $\text{ZrO}_2$ , mixed-oxide films. While the mixed oxides are used in today's automotive catalysts, the surface areas are reported to drop below  $2\text{ m}^2/\text{g}$  [39,40]. Maintaining a higher surface area could enhance the properties of the mixed oxide. In another example, researchers at Daihatsu reported that perovskite-supported catalysts can exhibit very attractive properties [41,42]; however, because most perovskite powders have very low surface areas, it may not be possible to take full advantage of this fact. Preparation of a perovskite film on a support could allow the attractive properties of the perovskite to be used to full advantage.

Clearly, the concept of preparing functional catalysts supports by ALD is still in its infancy. However, we believe this approach could result in catalysts with improved performance and stability.

## 5. Conclusions

Deposition of  $\text{CeO}_2$  by ALD can be used to form thin, conformal films on porous  $\text{Al}_2\text{O}_3$ , and the composites formed in this way can be used as catalyst supports for Pd. The supported-Pd catalysts prepared from the ALD-modified supports exhibit similar water-gas-shift rates to those obtained on conventional Pd/ $\text{CeO}_2$  catalysts, implying that there is good contact between the Pd and the  $\text{CeO}_2$ . The ALD-prepared catalysts have much better thermal stability than conventional  $\text{CeO}_2$  supports due to the underlying  $\text{Al}_2\text{O}_3$ .

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